Mechanics of Materials 10th Edition, Hibbeler Solutions Manual
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2–1.

An air-filled rubber ball has a diameter of 6 in. If the air pressure within the ball is increased until the diameter becomes 7 in., determine the average normal strain in the rubber.

SOLUTION

 $d_0 = 6$ in. $d = 7$ in.

$$
a = 7 \,\mathrm{m}
$$

$$
\epsilon = \frac{\pi d - \pi d_0}{\pi d_0} = \frac{7 - 6}{6} = 0.167 \text{ in.}/\text{in.}
$$
 Ans.

2–2.

A thin strip of rubber has an unstretched length of 15 in. If it is stretched around a pipe having an outer diameter of 5 in., determine the average normal strain in the strip.

SOLUTION

 $L_0 = 15$ in. $L = \pi(5 \text{ in.})$ $\epsilon = \frac{L - L_0}{L_0} = \frac{5\pi - 15}{15} = 0.0472 \text{ in.}/\text{in.}$ Ans.

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> > **Ans:** $\epsilon = 0.0472$ in./in.

2–3.

If the load **P** on the beam causes the end *C* to be displaced 10 mm downward, determine the normal strain in wires *CE* and *BD*.

 ϵ_{CE} = 0.00250 mm/mm, ϵ_{BD} = 0.00107 mm/mm

***2–4.**

The force applied at the handle of the rigid lever causes the lever to rotate clockwise about the pin *B* through an angle of 2°. Determine the average normal strain in each wire. The wires are unstretched when the lever is in the horizontal position.

SOLUTION

Geometry: The lever arm rotates through an angle of $\theta = \left(\frac{2^{\circ}}{180}\right)\pi$ rad = 0.03491 rad. Since θ is small, the displacements of points A , C , and D can be approximated by

 δ_A = 200(0.03491) = 6.9813 mm

- $\delta_C = 300(0.03491) = 10.4720$ mm
- δ_D = 500(0.03491) = 17.4533 mm

Average Normal Strain: The unstretched length of wires *AH*, *CG*, and *DF* are

 L_{AH} = 200 mm, L_{CG} = 300 mm, and L_{DF} = 300 mm. We obtain

$$
(\epsilon_{\text{avg}})_{AH} = \frac{\delta_A}{L_{AH}} = \frac{6.9813}{200} = 0.0349 \text{ mm/mm}
$$
\n
$$
(\epsilon_{\text{avg}})_{CG} = \frac{\delta_C}{L_{CG}} = \frac{10.4720}{300} = 0.0349 \text{ mm/mm}
$$
\n
$$
(\epsilon_{\text{avg}})_{DF} = \frac{\delta_D}{L_{DF}} = \frac{17.4533}{300} = 0.0582 \text{ mm/mm}
$$
\n
$$
\frac{\delta_D}{\delta_{\text{avg}}}
$$
\n
$$
\frac{200 \text{ mm}}{200 \text{ mm}}
$$

 (a)

Ans: $(\epsilon_{\text{avg}})_{AH} = 0.0349$ mm/mm $(\epsilon_{\text{avg}})_{CG} = 0.0349 \text{ mm/mm}$ $(\epsilon_{\text{avg}})_{DF} = 0.0582 \text{ mm/mm}$

2–5.

The rectangular plate is subjected to the deformation shown by the dashed line. Determine the average shear strain γ_{xy} in the plate.

SOLUTION

Geometry:

$$
\theta' = \tan^{-1} \frac{3}{150} = 0.0200 \text{ rad}
$$

$$
\theta = \left(\frac{\pi}{2} + 0.0200\right) \text{ rad}
$$

Shear Strain:

^g*xy* ⁼ ^p ² - ^u ⁼ ^p ² - ^a p 2 + 0.0200b = -0.0200 rad **Ans.** This work is protected by United States copyright laws and is provided solely for the use of instructors in teaching their courses and assessing student learning. Dissemination or sale of any part of this work (including on the World Wide Web) will destroy the integrity of the work and is not permitted.

2–6.

The square deforms into the position shown by the dashed lines. Determine the shear strain at each of its corners, *A*, *B*, *C*, and *D,* relative to the *x*, *y* axes. Side *D*′*B*′ remains horizontal.

SOLUTION

Geometry:

$$
B'C' = \sqrt{(8+3)^2 + (53 \sin 88.5^\circ)^2} = 54.1117 \text{ mm}
$$

\n
$$
C'D' = \sqrt{53^2 + 58^2 - 2(53)(58) \cos 91.5^\circ}
$$

\n
$$
= 79.5860 \text{ mm}
$$

\n
$$
B'D' = 50 + 53 \sin 1.5^\circ - 3 = 48.3874 \text{ mm}
$$

\n
$$
\cos \theta = \frac{(B'D')^2 + (B'C')^2 - (C'D')^2}{2(B'D')(B'C')}
$$

\n
$$
= \frac{48.3874^2 + 54.1117^2 - 79.5860^2}{2(48.3874)(54.1117)} = -0.20328
$$

\n
$$
\theta = 101.73^\circ
$$

\n
$$
\beta = 180^\circ - \theta = 78.27^\circ
$$

Shear Strain:

$$
\theta = 101.73^{\circ}
$$
\n
$$
\theta = 101.73^{\circ}
$$
\n
$$
\beta = 180^{\circ} - \theta = 78.27^{\circ}
$$
\n
$$
\alpha_{\text{min}}
$$
\n
$$
(\gamma_A)_{xy} = \frac{\pi}{2} - \pi \left(\frac{91.5^{\circ}}{180^{\circ}}\right) = -0.0262 \text{ rad}
$$
\n
$$
(\gamma_C)_{xy} = \beta - \frac{\pi}{2} = \pi \left(\frac{78.27^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
(\gamma_D)_{xy} = \pi \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
(\gamma_D)_{xy} = \pi \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
(\gamma_D)_{xy} = \pi \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
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(\gamma_D)_{xy} = \pi \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
(\gamma_D)_{xy} = \pi \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
\gamma_D = \frac{\pi}{2} \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$
\n
$$
\gamma_D = \frac{\pi}{2} \left(\frac{88.5^{\circ}}{180^{\circ}}\right) - \frac{\pi}{2} = -0.0262 \text{ rad}
$$

A 50 mm 8 mm 50 mm 3 mm 53 mm *D x ^D*¿ *^B C C*¿ *B*¿ 91.5

y

Ans:

 $(\gamma_A)_{xy} = -0.0262 \text{ rad}$ $(\gamma_B)_{xy} = -0.205$ rad $(\gamma_C)_{xy} = -0.205$ rad $(\gamma_D)_{xy} = -0.0262 \text{ rad}$

2–7.

The pin-connected rigid rods *AB* and *BC* are inclined at $\theta = 30^{\circ}$ when they are unloaded. When the force **P** is applied θ becomes 30.2°. Determine the average normal strain in wire *AC*.

SOLUTION

Geometry: Referring to Fig. *a*, the unstretched and stretched lengths of wire *AD* are

 L_{AC} = 2(600 sin 30°) = 600 mm

 $L_{AC'}$ = 2(600 sin 30.2°) = 603.6239 mm

Average Normal Strain:

2–9.

If a horizontal load applied to the bar *AC* causes point *A* to be displaced to the right by an amount ∆*L*, determine the normal strain in the wire *AB*. Originally, $\theta = 45^{\circ}$.

SOLUTION

$$
L'_{AB} = \sqrt{(\sqrt{2}L)^2 + \Delta L^2 - 2(\sqrt{2}L)(\Delta L)\cos 135^\circ}
$$

= $\sqrt{2L^2 + \Delta L^2 + 2L\Delta L}$

$$
\epsilon_{AB} = \frac{L'_{AB} - L_{AB}}{L_{AB}}
$$

= $\frac{\sqrt{2L^2 + \Delta L^2 + 2L\Delta L} - \sqrt{2}L}{\sqrt{2}L}$
= $\sqrt{1 + \frac{\Delta L^2}{2L^2} + \frac{\Delta L}{L}} - 1$

Neglecting the higher-order terms,

$$
\epsilon_{AB} = \left(1 + \frac{\Delta L}{L}\right)^{\frac{1}{2}} - 1
$$
\n
$$
\epsilon_{AB} = \left(1 + \frac{\Delta L}{L}\right)^{\frac{1}{2}} - 1
$$
\n
$$
= 1 + \frac{1}{2} \frac{\Delta L}{L} + \dots - 1
$$
\n
$$
= \frac{0.5 \Delta L}{L}
$$
\n
$$
\epsilon_{AB} = \frac{\Delta L \sin 45^{\circ}}{\pi} = \frac{0.5 \Delta L}{L}
$$
\nAns.

Also,

$$
\epsilon_{AB} = \frac{\Delta L \sin 45^\circ}{\sqrt{2}L} = \frac{0.5 \Delta L}{L}
$$
Ans.

L

B θ

 $\frac{C}{2}$ *A L*

 450

 $\frac{1}{\Delta L}$

Ans.

Ans.

2–10.

Determine the shear strain γ_{xy} at corners *A* and *B* if the plastic distorts as shown by the dashed lines.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*, the small-angle analysis gives

$$
\alpha = \psi = \frac{7}{306} = 0.022876 \text{ rad}
$$

$$
\beta = \frac{5}{408} = 0.012255 \text{ rad}
$$

$$
\theta = \frac{2}{405} = 0.0049383 \text{ rad}
$$

Shear Strain: By definition,

$$
(\gamma_A)_{xy} = \theta + \psi = 0.02781 \text{ rad} = 27.8(10^{-3}) \text{ rad}
$$

$$
(\gamma_B)_{xy} = \alpha + \beta = 0.03513 \text{ rad} = 35.1(10^{-3}) \text{ rad}
$$

Ans: $(\gamma_A)_{xy} = 27.8(10^{-3})$ rad $(\gamma_B)_{xy} = 35.1(10^{-3})$ rad

2–11.

Determine the shear strain γ_{xy} at corners *D* and *C* if the plastic distorts as shown by the dashed lines.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*, the small-angle analysis gives

$$
\alpha = \psi = \frac{4}{303} = 0.013201 \text{ rad}
$$

$$
\theta = \frac{2}{405} = 0.0049383 \text{ rad}
$$

$$
\beta = \frac{5}{408} = 0.012255 \text{ rad}
$$

Shear Strain: By definition,

$$
(\gamma_{xy})_C = \alpha + \beta = 0.02546 \text{ rad} = 25.5(10^{-3}) \text{ rad}
$$

\n $(\gamma_{xy})_D = \theta + \psi = 0.01814 \text{ rad} = 18.1(10^{-3}) \text{ rad}$

$$
(\gamma_{xy})_C = \alpha + \beta = 0.02546 \text{ rad} = 25.5(10^{-3}) \text{ rad}
$$
\n
$$
(\gamma_{xy})_D = \theta + \psi = 0.01814 \text{ rad} = 18.1(10^{-3}) \text{ rad}
$$
\n
$$
\frac{d}{dx}
$$
\

Ans: $(\gamma_{xy})_C = 25.5(10^{-3})$ rad $(y_{xy})_D = 18.1(10^{-3})$ rad

***2–12.**

The material distorts into the dashed position shown. Determine the average normal strains ϵ_x , ϵ_y and the shear strain γ_{xy} at *A*, and the average normal strain along line *BE*.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*,

$$
\tan \theta = \frac{15}{250}; \qquad \theta = (3.4336^\circ) \left(\frac{\pi}{180^\circ} \text{ rad}\right) = 0.05993 \text{ rad}
$$
\n
$$
L_{AC}' = \sqrt{15^2 + 150^2} = \sqrt{62725} \text{ mm}
$$
\n
$$
\frac{BB'}{15} = \frac{200}{250}; \qquad BB' = 12 \text{ mm} \qquad \frac{EE'}{30} = \frac{50}{250}; \qquad EE' = 6 \text{ mm}
$$
\n
$$
x' = 150 + EE' - BB' = 150 + 6 - 12 = 144 \text{ mm}
$$

$$
L_{BE} = \sqrt{150^2 + 150^2} = 150\sqrt{2} \text{ mm} \quad L_B'_{E'} = \sqrt{144^2 + 150^2} = \sqrt{43236} \text{ mm}
$$

Average Normal and Shear Strain: Since no deformation occurs along *x* axis,

$$
E_{z} = \sqrt{150^2 + 150^2} = 150\sqrt{2} \text{ mm } L_B'_{E'} = \sqrt{144^2 + 150^2} = \sqrt{43236} \text{ mm}
$$
\n
$$
E_{A} = \sqrt{62725 - 250} = 1.80(10^{-3}) \text{ mm/mm}^2/\text{m}^
$$

By definition,

$$
(\gamma_{xy})_A = \theta = 0.0599 \text{ rad}
$$

$$
\epsilon_{BE} = \frac{L_{B'E'} - L_{BE}}{L_{BE}} = \frac{\sqrt{43236} - 150\sqrt{2}}{150\sqrt{2}} \approx 0.0198 \text{ mm/mm}
$$

Ans: $(\epsilon_x)_A = 0$ $(\epsilon_y)_A = 1.80(10^{-3})$ mm/mm $(\gamma_{xy})_A = 0.0599$ rad ϵ_{BE} = -0.0198 mm/mm

x

50 mm

Ť. J

y

B

C

50 mm

200 mm

 $A \longleftarrow 150 \text{ mm} \longrightarrow F$

E

15 mm 30 mm *D*

2–13.

The material distorts into the dashed position shown. Determine the average normal strains along the diagonals *AD* and *CF*.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*,

 $L_{AD} = L_{CF} = \sqrt{150^2 + 250^2} = \sqrt{85000}$ mm $L_{AD'} = \sqrt{(150 + 30)^2 + 250^2} = \sqrt{94900}$ mm $L_{C/F} = \sqrt{(150 - 15)^2 + 250^2} = \sqrt{80725}$ mm

Average Normal Strain:

Ans: $\epsilon_{AD} = 0.0566$ mm/mm ϵ_{CF} = -0.0255 mm/mm

x

50 mm

Ŧ T

y

B

C

50 mm

200 mm

 $A \longleftarrow 150 \text{ mm} \longrightarrow F$

15 mm 30 mm *D*

E

2–14.

Part of a control linkage for an airplane consists of a rigid member *CB* and a flexible cable *AB*. If a force is applied to the end *B* of the member and causes it to rotate by $\theta = 0.5^{\circ}$, determine the normal strain in the cable. Originally the cable is unstretched.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*, the unstretched and stretched lengths of cable *AB* are

$$
L_{AB} = \sqrt{600^2 + 800^2} = 1000 \text{ mm}
$$

$$
L_{AB'} = \sqrt{600^2 + 800^2 - 2(600)(800) \cos 90.5^\circ} = 1004.18 \text{ mm}
$$

Average Normal Strain:

600 mm

C

 $B \left(\bigotimes \right)$ **P**

 θ

800 mm

A

2–15.

Part of a control linkage for an airplane consists of a rigid member *CB* and a flexible cable *AB*. If a force is applied to the end *B* of the member and causes a normal strain in the cable of 0.004 mm/mm, determine the displacement of point *B*. Originally the cable is unstretched.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a*, the unstretched and stretched lengths of cable *AB* are

$$
L_{AB} = \sqrt{600^2 + 800^2} = 1000 \text{ mm}
$$

\n
$$
L_{AB'} = \sqrt{600^2 + 800^2 - 2(600)(800) \cos (90^\circ + \theta)}
$$

\n
$$
L_{AB'} = \sqrt{1(10^6) - 0.960(10^6) \cos (90^\circ + \theta)}
$$

Average Normal Strain:

^P*AB* ⁼ *LAB*′ - *LAB LAB* ;0.004 ⁼ ²1(106) - 0.960(106) cos (90° + u) - 1000 1000 ^u ⁼ 0.4784°^a ^p 180° b = 0.008350 rad and is provided solely for the use of instructors in teaching or sale of any part of this work (including on the World Wide Web)

Thus,

$$
\Delta_B = \theta L_{BC} = 0.008350(800) = 6.68 \text{ mm}
$$

600 mm

C

 $\overline{\mathcal{O}}$

 $B \left(\bigotimes \right)$ **P**

 θ

800 mm

A

P

 Δ_C

 B $\left(\begin{array}{ccc} & & & \\ \hline \mathcal{E} & & & D \end{array}\right)$

 Δ_D

L

A

***2–16.**

The nylon cord has an original length *L* and is tied to a bolt at *A* and a roller at *B*. If a force **P** is applied to the roller, determine the normal strain in the cord when the roller is at *C*, and at *D*. If the cord is originally unstrained when it is at *C*, determine the normal strain ϵ_D when the roller moves to *D*. Show that if the displacements Δ_C and Δ_D are small, then $\epsilon'_D = \epsilon_D - \epsilon_C$.

SOLUTION

$$
L_C = \sqrt{L^2 + \Delta_C^2}
$$

\n
$$
\epsilon_C = \frac{\sqrt{L^2 + \Delta_C^2} - L}{L}
$$

\n
$$
= \frac{L\sqrt{1 + \left(\frac{\Delta_C^2}{L}\right)} - L}{L} = \sqrt{1 + \left(\frac{\Delta_C^2}{L^2}\right)} - 1
$$

For small Δ_C ,

$$
\epsilon_C = 1 + \frac{1}{2} \left(\frac{\Delta_C^2}{L^2} \right) - 1 = \frac{1}{2} \frac{\Delta_C^2}{L^2}
$$
Ans.

In the same manner,

$$
\epsilon_C = 1 + \frac{1}{2} \left(\frac{\Delta_C}{L^2} \right) - 1 = \frac{1}{2} \frac{\Delta_C}{L^2}
$$
\nIn the same manner,
\n
$$
\epsilon_D = \frac{1}{2} \frac{\Delta_D^2}{L^2}
$$
\n
$$
\epsilon_D' = \frac{\sqrt{L^2 + \Delta_D^2} - \sqrt{L^2 + \Delta_C^2}}{\sqrt{L^2 + \Delta_C^2}} = \frac{\sqrt{1 + \frac{\Delta_D^2}{L^2} - \sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}}}{\sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}} = \frac{\sqrt{1 + \frac{\Delta_E^2}{L^2} - \sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}}}{\sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}} = \frac{\sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}}{\sqrt{1 + \frac{\Delta_E^2}{L^2} \cos \theta_0^2}} = \frac{1}{2L^2} (\Delta_C^2 + \Delta_D^2)
$$
\nFor small Δ_C and Δ_D ,
\n
$$
\epsilon_D' = \frac{\left(1 + \frac{1}{2} \frac{\Delta_C^2}{L^2}\right) - \left(1 + \frac{1}{2} \frac{\Delta_D^2}{L^2}\right)}{\left(1 + \frac{1}{2} \frac{\Delta_C^2}{L^2}\right)} = \frac{\frac{1}{2L^2} (\Delta_C^2 + \Delta_D^2)}{\frac{1}{2L^2} (2L^2 + \Delta_D^2)}
$$

For small Δ_C and Δ_D ,

$$
\epsilon_D' = \frac{\left(1 + \frac{1}{2}\frac{\Delta_C^2}{l^2}\right) - \left(1 + \frac{1}{2}\frac{\Delta_D^2}{l^2}\right)}{\left(1 + \frac{1}{2}\frac{\Delta_C^2}{l^2}\right)} = \frac{\frac{1}{2l^2}\left(\Delta_C^2 + \Delta_D^2\right)}{\frac{1}{2l^2}\left(2L^2 + \Delta_C^2\right)}\delta_C^{\text{max}}
$$
\n
$$
\epsilon_D' = \frac{\Delta_C^2 - \Delta_D^2}{2L^2 - \Delta_C^2} = \frac{1}{2L^2}\left(\Delta_C^2 - \Delta_D^2\right) = \epsilon_C - \epsilon_D
$$

Also this problem can be solved as follows:

$$
A_C = L \sec \theta_C; \qquad A_D = L \sec \theta_D
$$

$$
\epsilon_C = \frac{L \sec \theta_C - L}{L} = \sec \theta_C - 1
$$

$$
L \sec \theta_D - L
$$

$$
\epsilon_D = \frac{L \sec \theta_D - L}{L} = \sec \theta_D - 1
$$

Expanding sec θ

 $\sec \theta = 1 + \frac{\theta^2}{2!}$ $\frac{\theta^2}{2!} + \frac{5 \theta^4}{4!}$ ²) = P*^C* - P*^D* **QED**

***2–16. Continued**

For small θ neglect the higher order terms

$$
\sec \theta = 1 + \frac{\theta^2}{2}
$$

Hence,

 $\epsilon_C = 1 + \frac{\theta_C^2}{2} - 1 = \frac{\theta_C^2}{2}$ 2 $\epsilon_D = 1 + \frac{\theta_D^2}{2} - 1 = \frac{\theta_D^2}{2}$ 2 $\epsilon_D' = \frac{L \sec \theta_D - L \sec \theta_C}{L \sec \theta_C} = \frac{\sec \theta_D}{\sec \theta_C} - 1 = \sec \theta_D \cos \theta_C - 1$ Since $\cos \theta = 1 - \frac{\theta^2}{2!} + \frac{\theta^4}{4!}$ sec $\theta_D \cos \theta_C = \left(1 + \frac{\theta_D^2}{2} \dots \right) \left(1 - \frac{\theta_C^2}{2}\right)$ $\frac{c}{2}$ $= 1 - \frac{\theta_C^2}{2}$ $\frac{\theta_{C}^{2}}{2} + \frac{\theta_{D}^{2}}{2} - \frac{\theta_{C}^{2} \theta_{D}^{2}}{4}$ 4 The and of the protected by the back is protected by the copyright laws and the copyright laws of the copyright laws of the copyright laws and the copyright laws and the copyright laws and the copyright laws and the copyri and is provided solely for the use of the use the courses and assessment learning to the courses of the sec $\theta_D \cos \theta_C - 1$

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Neglecting the higher order terms

Neglecting the higher order terms
\n
$$
\sec \theta_D \cos \theta_C = 1 + \frac{\theta_D^2}{2} - \frac{\theta_C^2}{2}
$$
\n
$$
\epsilon_D' = \left[1 + \frac{\theta_2^2}{2} - \frac{\theta_1^2}{2}\right] - 1 = \frac{\theta_D^2}{2} - \frac{\theta_C^2}{2}
$$
\n
$$
= \epsilon_D - \epsilon_C
$$
\nQED

Ans: $\epsilon_C = \frac{1}{2}$ Δ_C^2 L^2 $\epsilon_D = \frac{1}{2}$ Δ_D^2 L^2

2–17.

A thin wire, lying along the *x* axis, is strained such that each point on the wire is displaced $\Delta x = kx^2$ along the *x* axis. If *k* is constant, what is the normal strain at any point *P* along the wire?

SOLUTION

$$
\epsilon = \frac{d(\Delta x)}{dx} = 2 k x
$$
 Ans.

2–18.

***2–20.**

Determine the average normal strain that occurs along the diagonals *AC* and *DB*.

SOLUTION

Geometry:

 $AC = DB = \sqrt{400^2 + 300^2} = 500$ mm $DB' = \sqrt{405^2 + 304^2} = 506.4$ mm $A'C' = \sqrt{401^2 + 300^2} = 500.8$ mm

Average Normal Strain:

$$
\epsilon_{AC} = \frac{A'C' - AC}{AC} = \frac{500.8 - 500}{500}
$$

= 0.00160 mm/mm = 1.60(10⁻³) mm/mm

$$
\epsilon_{DB} = \frac{DB' - DB}{DB} = \frac{506.4 - 500}{500}
$$

= 0.0128 mm/mm = 12.8(10⁻³) mm/mm

$$
\epsilon_{DB} = \frac{0.0128 \text{ mm/mm}}{0.0128 \text{ mm/mm}} = 12.8(10-3) \text{ mm/mm}
$$

$$
2 \text{ mm} \left[C \left| \frac{2 \text{ mm}}{C} \right| \right] = 2 \text{ mm}
$$
\n
$$
300 \text{ mm}
$$
\n
$$
300 \text{ mm}
$$
\n
$$
400 \text{ mm}
$$
\n
$$
3 \text{ mm}
$$

Ans: $\epsilon_{AC} = 1.60(10^{-3})$ mm/mm $\epsilon_{DB} = 12.8(10^{-3})$ mm/mm

2–21.

The corners of the square plate are given the displacements indicated. Determine the average normal strains ϵ_x and ϵ_y along the *x* and *y* axes.

SOLUTION

$$
\epsilon_x = \frac{-0.3}{10} = -0.03 \text{ in.}/\text{in.}
$$
Ans.

Ans: $\epsilon_x = -0.03$ in./in. $\epsilon_y = 0.02$ in./in.

2–22.

The triangular plate is fixed at its base, and its apex *A* is given a horizontal displacement of 5 mm. Determine the shear strain, γ_{xy} , at *A*.

SOLUTION

 $L = \sqrt{800^2 + 5^2 - 2(800)(5) \cos 135^\circ} = 803.54 \text{ mm}$ $\frac{\sin 135^{\circ}}{803.54} = \frac{\sin \theta}{800}; \qquad \theta = 44.75^{\circ} = 0.7810 \text{ rad}$

$$
\gamma_{xy} = \frac{\pi}{2} - 2\theta = \frac{\pi}{2} - 2(0.7810)
$$

= 0.00880 rad **Ans.**

x

x¿

y

 45°

800 mm

A

45 45

A¿ 5 mm

800 mm

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***2–24.**

The triangular plate is fixed at its base, and its apex *A* is given a horizontal displacement of 5 mm. Determine the average normal strain $\epsilon_{x'}$ along the *x'* axis.

SOLUTION

$$
L = 800 \cos 45^{\circ} = 565.69 \text{ mm}
$$

$$
\epsilon_{x'} = \frac{5}{565.69} = 0.00884 \text{ mm/mm}
$$

Ans: $\epsilon_{\mathbf{x}'} = 0.00884$ mm/mm

2–25.

The polysulfone block is glued at its top and bottom to the rigid plates. If a tangential force, applied to the top plate, causes the material to deform so that its sides are described by the equation $y = 3.56 x^{1/4}$, determine the shear strain at

y **P** *B* the corners *A* and *B*. $y = 3.56 x^{1/4}$ *^A ^D* $\frac{8}{2}$ $\frac{du}{dy} = 0$ **Ans.** Analysis of the order of the decline of th $\frac{dx}{dy} = 1.123(0.0996)^{3/4} = 0.199 \text{ rad}$ Ans.

Ans: $\gamma_A = 0$ $\gamma_B = 0.199$ rad

C

2 in.

x

SOLUTION

$$
y = 3.56 x^{1/4}
$$

$$
\frac{dy}{dx} = 0.890 x^{-3/4}
$$

$$
\frac{dx}{dy} = 1.123 x^{3/4}
$$

At $A, x = 0$

$$
\gamma_A = \frac{dx}{dy} = 0
$$

At *B*,

$$
2 = 3.56 x^{1/4}
$$

 $x = 0.0996$ in.

$$
\gamma_B = \frac{dx}{dy} = 1.123(0.0996)^{3/4} = 0.199
$$
 rad

2–26.

The corners of the square plate are given the displacements indicated. Determine the shear strain at *A* relative to axes that are directed along *AB* and *AD*, and the shear strain at *B* relative to axes that are directed along *BC* and *BA.*

SOLUTION

 $11.5h$

 $11.5in$

Geometry: Referring to the geometry shown in Fig. *a,*

$$
\tan\frac{\theta}{2} = \frac{12.3}{11.5} \qquad \theta = (93.85^\circ) \left(\frac{\pi}{180^\circ} \text{ rad}\right) = 1.6380 \text{ rad}
$$

$$
\tan\frac{\phi}{2} = \frac{11.5}{12.3} \qquad \phi = (86.15^\circ) \left(\frac{\pi}{180^\circ} \text{ rad}\right) = 1.5036 \text{ rad}
$$

Shear Strain: By definition,

$$
(\gamma_{x'y'})_A = \frac{\pi}{2} - \theta = \frac{\pi}{2} - 1.6380 = -0.0672 \text{ rad}
$$
Ans.
\n
$$
(\gamma_{x'y'})_B = \frac{\pi}{2} - \phi = \frac{\pi}{2} - 1.5036 = 0.0672 \text{ rad}
$$

 $rac{\Theta}{\Sigma}$ '∡′

 $12.3\,\pi$

 (a)

 $12.3n$

Ans:

$$
(\gamma_{\text{min}})_{4} = -0.06
$$

 $(\gamma_{x'y'})_A = -0.0672$ rad $(\gamma_{x''y''})_B = 0.0672$ rad

Will destroy the integrity of the work and is not permitted.

2–27.

The corners of the square plate are given the displacements indicated. Determine the average normal strains along side *AB* and diagonals *AC* and *BD*. 0.3 in.

SOLUTION

Geometry: Referring to the geometry shown in Fig. *a,*

 $L_{AB} = \sqrt{12^2 + 12^2} = 12\sqrt{2}$ in. $L_{A'B'} = \sqrt{12.3^2 + 11.5^2} = \sqrt{283.54}$ in. $L_{BD} = 2(12) = 24$ in. $L_{B'D'}$ = 2(12 + 0.3) = 24.6 in. $L_{AC} = 2(12) = 24$ in.

$$
L_{A}{}'_{C}{}' = 2(12 - 0.5) = 23 \text{ in.}
$$

Average Normal Strain:

$$
\epsilon_{AB} = \frac{L_{A'B'} - L_{AB}}{L_{AB}} = \frac{\sqrt{283.54} - 12\sqrt{2}}{12\sqrt{2}} = -7.77(10^{39} \text{ in.})\text{ in.}
$$
\n
$$
\epsilon_{BD} = \frac{L_{B'D'} - L_{BD}}{L_{BD}} = \frac{24.6 - 24}{24} = 0.025 \text{ in.}
$$
\n
$$
\epsilon_{AC} = \frac{L_{A'C'} - L_{AC}}{L_{AC}} = \frac{23 - 24}{24} = -0.0417 \text{ in.}
$$
\n
$$
\epsilon_{AC} = \frac{L_{A'C'} - L_{AC}}{24} = \frac{23 - 24}{24} = -0.0417 \text{ in.}
$$
\nAns.

132

***2–28.**

The block is deformed into the position shown by the dashed lines. Determine the average normal strain along line *AB*.

SOLUTION

Geometry:

 $AB = \sqrt{100^2 + (70 - 30)^2} = 107.7033$ mm $AB' = \sqrt{(70 - 30 - 15)^2 + (110^2 - 15^2)} = 111.8034$ mm

Average Normal Strain:

$$
\epsilon_{AB} = \frac{AB' - AB}{AB}
$$

$$
=\frac{111.8034-107.7033}{107.7033}
$$

 $= 0.0381 \text{ mm/mm} = 38.1 (10^{-3}) \text{ mm}$

Ans:

$$
\epsilon_{AB} = 38.1 (10^{-3}) \text{ mm}
$$

2–29.

The rectangular plate is deformed into the shape shown by the dashed lines. Determine the average normal strain along diagonal *AC*, and the average shear strain at corner *A* relative to the *x*, *y* axes.

SOLUTION

Geometry: The unstretched length of diagonal *AC* is

$$
L_{AC} = \sqrt{300^2 + 400^2} = 500 \text{ mm}
$$

Referring to Fig. *a*, the stretched length of diagonal *AC* is

$$
L_{AC'} = \sqrt{(400 + 6)^2 + (300 + 6)^2} = 508.4014 \text{ mm}
$$

Referring to Fig. *a* and using small angle analysis,

$$
\phi = \frac{2}{300 + 2} = 0.006623 \text{ rad}
$$

$$
\alpha = \frac{2}{400 + 3} = 0.004963 \text{ rad}
$$

Average Normal Strain: Applying Eq. 2,

$$
\alpha = \frac{2}{400 + 3} = 0.004963 \text{ rad}
$$
\n
$$
\text{range Normal Strain: Applying Eq. 2,}
$$
\n
$$
(\epsilon_{\text{avg}})_{AC} = \frac{L_{AC} - L_{AC}}{L_{AC}} = \frac{508.4014 - 500}{500} = 0.0168 \text{ mm/min} \text{ mm}^{-1}
$$
\n
$$
(\gamma_A)_{xy} = \phi + \alpha = 0.006623 + 0.004963 = 0.0116 \text{ rad}^{-1}
$$
\nAns.

Shear Strain: Referring to Fig. *a*,

$$
(\gamma_A)_{xy} = \phi + \alpha = 0.006623 + 0.004963 = 0.0116 \text{ rad} \text{ rad} \text{ rad} \text{ s}^{-1}
$$

$$
2mm
$$
\n
$$
400mm
$$
\n
$$
3mm
$$
\n
$$
(a)
$$

Ans: $(\epsilon_{avg})_{AC} = 0.0168$ mm/mm, $(\gamma_A)_{xy} = 0.0116$ rad

2–30.

The rectangular plate is deformed into the shape shown by the dashed lines. Determine the average normal strain along diagonal *BD*, and the average shear strain at corner *B* relative to the *x*, *y* axes.

SOLUTION

Geometry: The unstretched length of diagonal *BD* is

$$
L_{BD} = \sqrt{300^2 + 400^2} = 500 \text{ mm}
$$

Referring to Fig. *a*, the stretched length of diagonal *BD* is

$$
L_{B'D'} = \sqrt{(300 + 2 - 2)^2 + (400 + 3 - 2)^2} = 500.8004 \text{ mm}
$$

Referring to Fig. *a* and using small angle analysis,

$$
\phi = \frac{2}{403} = 0.004963 \text{ rad}
$$

$$
\alpha = \frac{3}{300 + 6 - 2} = 0.009868 \text{ rad}
$$

Average Normal Strain: Applying Eq. 2,

$$
\alpha = \frac{3}{300 + 6 - 2} = 0.009868 \text{ rad}
$$

\n**Normal Strain:** Applying Eq. 2,
\n
$$
(\epsilon_{\text{avg}})_{BD} = \frac{L_{B'D'} - L_{BD}}{L_{BD}} = \frac{500.8004 - 500}{500} = 1.60(10^{-3}) \text{mm/mm} \text{ Ans.}
$$
\n
\n**train:** Referring to Fig. a,
\n
$$
(\gamma_B)_{xy} = \phi + \alpha = 0.004963 + 0.009868 = 0.0148 \text{ rad}^{\text{tot}}
$$
\nAns.
\n
$$
\gamma_B = \frac{1}{\sqrt{3}} = \frac{0.004963 + 0.009868}{0.0148 \text{ rad}^{\text{tot}}}
$$
\nAns.

Shear Strain: Referring to Fig. *a*,

$$
(\gamma_B)_{xy} = \phi + \alpha = 0.004963 + 0.009868 = 0.0148 \text{ rad}^3
$$

$$
\frac{2mn}{\frac{2mn}{D}}
$$
\n
$$
\frac{2mn}{D}
$$
\n
$$
\frac{2mn}{D}
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\n
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\n
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\frac{2mn}{2mn}
$$
\n
$$
\frac{2mn}{200mn}
$$
\n
$$
\frac{2mn}{200mn}
$$
\n
$$
\frac{2mn}{2mn}
$$
\n
$$
\frac{2mn}{2mn}
$$

$$
(a_{\,})
$$

Ans: $(\epsilon_{\text{avg}})_{BD} = 1.60(10^{-3})$ mm/mm, $(\gamma_B)_{xy} = 0.0148 \text{ rad}$

2–31.

The nonuniform loading causes a normal strain in the shaft that can be expressed as $\epsilon_x = k \sin\left(\frac{\pi}{L}x\right)$, where *k* is a constant. Determine the displacement of the center *C* and the average normal strain in the entire rod.

$\frac{L}{2}$ $\frac{L}{2}$ \longrightarrow $\frac{L}{2}$ 2 *A B C*

SOLUTION

***2–32.**

The rectangular plate undergoes a deformation shown by the dashed lines. Determine the shear strain γ_{xy} and $\gamma_{x'y'}$ at point *A*.

SOLUTION

 $\tan \theta = \frac{5.02}{4.99}$

 $\gamma_{x'y'} = \frac{\pi}{2} - 2\theta$

 $\theta = 45.17^{\circ} = 0.7884$ rad

 $= \frac{\pi}{2} - 2(0.7884)$

Since the right angle of an element along the *x*,*y* axes does not distort, then

A

 u_A *A*

L

 θ

x

B¿

B v*B*

y

2–33.

The fiber AB has a length L and orientation θ . If its ends A and *B* undergo very small displacements u_A and v_B respectively, determine the normal strain in the fiber when it is in position *A*′ *B*′.

SOLUTION

Geometry:

$$
L_{A'B'} = \sqrt{(L \cos \theta - u_A)^2 + (L \sin \theta + v_B)^2}
$$

= $\sqrt{L^2 + u_A^2 + v_B^2 + 2L(v_B \sin \theta - u_A \cos \theta)}$

Average Normal Strain:

$$
\epsilon_{AB} = \frac{L_{A'B'} - L}{L}
$$

= $\sqrt{1 + \frac{u_A^2 + v_B^2}{L^2} + \frac{2(v_B \sin \theta - u_A \cos \theta)}{L}} - 1$

Neglecting higher terms u_A^2 and v_B^2

$$
\epsilon_{AB} = \left[1 + \frac{2(v_B \sin \theta - u_A \cos \theta)}{L}\right]^{\frac{1}{2}} - 1
$$

Using the binomial theorem:

$$
= \sqrt{1 + \frac{u_A^2 + v_B^2}{L^2} + \frac{2(v_B \sin \theta - u_A \cos \theta)}{L} - 1}
$$

\nNeglecting higher terms u_A^2 and v_B^2
\n
$$
\epsilon_{AB} = \left[1 + \frac{2(v_B \sin \theta - u_A \cos \theta)}{L}\right]^{\frac{1}{2}} - 1
$$

\nUsing the binomial theorem:
\n
$$
\epsilon_{AB} = 1 + \frac{1}{2} \left(\frac{2v_B \sin \theta}{L} - \frac{2u_A \cos \theta}{L}\right) + \dots - 1
$$

\n
$$
= \frac{v_B \sin \theta}{L} - \frac{u_A \cos \theta}{L}
$$

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2–34.

If the normal strain is defined in reference to the final length ∆*s*′, that is,

$$
\epsilon' = \lim_{\Delta s' \to 0} \left(\frac{\Delta s' - \Delta s}{\Delta s'} \right)
$$

instead of in reference to the original length, Eq. 2–2, show that the difference in these strains is represented as a second-order term, namely, $\epsilon - \epsilon' = \epsilon \epsilon'$.

SOLUTION

$$
\epsilon = \frac{\Delta s' - \Delta s}{\Delta s}
$$
\n
$$
\epsilon - \epsilon' = \frac{\Delta s' - \Delta s}{\Delta s} - \frac{\Delta s' - \Delta s}{\Delta s'}
$$
\n
$$
= \frac{\Delta s'^2 - \Delta s \Delta s' - \Delta s' \Delta s + \Delta s^2}{\Delta s \Delta s'}
$$
\n
$$
= \frac{\Delta s'^2 + \Delta s^2 - 2\Delta s' \Delta s}{\Delta s \Delta s'}
$$
\n
$$
= \frac{(\Delta s' - \Delta s)^2}{\Delta s \Delta s'} = \left(\frac{\Delta s' - \Delta s}{\Delta s}\right) \left(\frac{\Delta s' - \Delta s}{\Delta s'}\right)
$$
\n
$$
= \epsilon \epsilon'
$$
\n(Q.E.D)

\n(Q.E.D)

\n(Q.E.D)

\n(Q.E.D)